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# Groundwater contamination risks from conservative point source pollutants in a future climate

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## ABSTRACT

The groundwater contamination risk in future climates was investigated at three locations in Sweden. Solute transport penetration depths were simulated using the HYDRUS-1D model using historical data and an ensemble of climate projections including two global climate models (GCMs), three emission scenarios and one regional climate model. Most projections indicated increasing precipitation and evapotranspiration until mid-century with a further increase at end-century. Results showed both increasing and decreasing groundwater contamination risks depending on emission scenario and GCM. Generally, the groundwater contamination risk is likely to be unchanged until mid-century, but higher at the end of the century. Soil and site specific relationships between  $\Delta(P - PET)$  (i.e. change in the difference between precipitation,  $P$ , and potential evapotranspiration,  $PET$ ) and changes in solute transport depths were determined. Using this, changes in solute transport depths for other climate projections can be assessed.

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## Introduction

The vadose zone acts as a filter, protecting ground water resources from pollutants spread on the soil surface. Assessing the risk for pollutants reaching the groundwater through the vadose zone is essential for protecting valuable groundwater resources. Pollutants can come from either point or diffuse sources. In very general terms, pollutants spread from non-point sources typically have lower concentrations and are less toxic compared to pollutants spread from point sources (e.g. Corwin 1996). Examples of point source pollutants are accidental spills of toxic substances, which are generally spread at relatively high concentrations over a limited area during a short period. Solute displacement through the unsaturated zone down to the groundwater is forced by infiltrated rainfall, snow melt or irrigation. The amount of excess precipitation (precipitation subtracted by actual evapotranspiration) and the temporal distribution of the precipitation will determine the depth of solute penetration, or the solute transport velocity. The intrinsic groundwater vulnerability depends on the likelihood of a pollutant reaching the groundwater due to the hydro-geological conditions. High solute transport velocities, or correspondingly, deep solute penetration depths, lead to an elevated risk for a pollutant spread at the soil surface to reach the groundwater table, thus increasing the vulnerability (e.g. Aller *et al.* 1987).

Several studies have confirmed the connection between high-intensity rainfall and macropore flow (e.g. Tiktak *et al.* 2004, Jarvis 2007, McGrath *et al.* 2010). Jarvis (2007) attributed this link to an enhanced macropore flow following high-intensity rainfall, by the ability of larger macropores to conduct water. Increasing rainfall intensity will lead to an increase also in pore

water velocity, which in turn will reduce solute traveling time. It is obvious that rainfall intensity plays a key role in solute movement through macropores and that this process is well understood. Macropore flow is, undoubtedly, important in many soils. However, in soils with low clay content matrix flow still governs the solute movement process (Koestel and Jorda 2014). Also for matrix flow there is a connection between the temporal variability of infiltration and solute transport depths. This has been shown both experimentally and numerically (e.g. Persson and Saifadeen 2016). However, the connection between rainfall variability and solute transport velocities for matrix flow is not as straightforward as for macropore flow. For example, a low temporal variability (steady-state) irrigation can lead to faster solute transport velocities compared to intermittent irrigation (see, e.g. Sharma and Taniguchi 1991, Persson and Berndtsson 1999), but a high temporal variability of natural rainfall may also lead to faster transport (e.g. Bicki and Guo 1991, Persson and Saifadeen 2016). Thus, more research is needed in this field.

The predicted effects of climate change will lead to a changed risk for groundwater contamination. For example, global climate models (GCMs) predict a future change in the rainfall dynamics for many regions of the world with resulting higher maximum rainfall intensities, longer drought periods between rainfall events and a higher annual rainfall amount (IPCC 2013). In addition, changes in potential evapotranspiration will have a significant impact on soil water content dynamics and root water uptake rates. The predicted changes are likely to affect solute transport rates through the unsaturated zone. A logical way of assessing climate change impacts is using climate model output as input in water and solute transport models. However, there are only a few published

studies that have estimated the change in solute transport (Arheimer *et al.* 2005, Olsson *et al.* 2016) or soil moisture distribution (Knapp *et al.* 2008, Gu and Riley 2010, Thomey *et al.* 2012; Stuart *et al.* 2012) for future rainfall climates. Knapp *et al.* (2008), based on both numerical and experimental results, concluded that future higher intensity rainfalls separated with longer dry periods would lead to a higher temporal variability of soil moisture in the top soil. This will, in turn, also affect solute transport velocities.

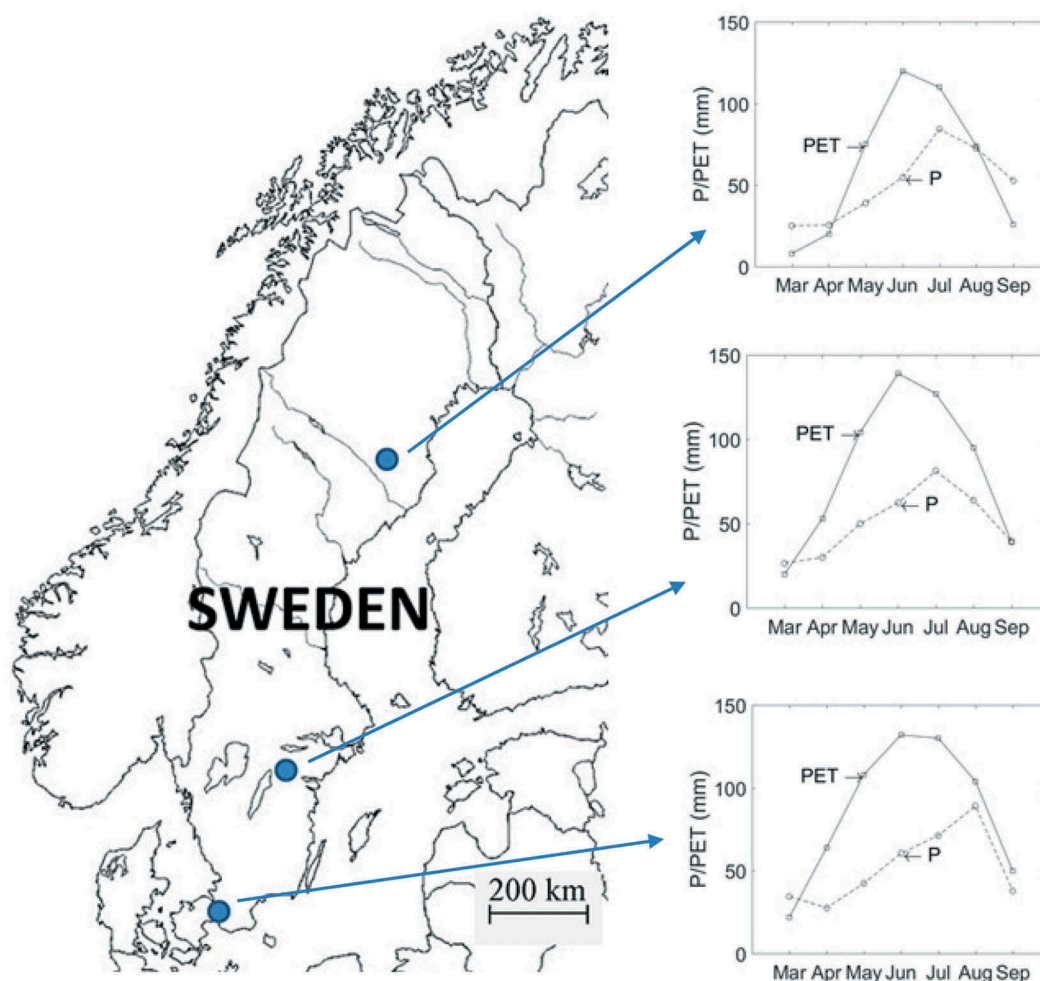
In order to accurately estimate the impacts of climate change on solute transport, detailed studies are required. For hydrological climate change impact assessment, a modelling scheme (or chain) has become state-of-the-art, where GCM output (mainly precipitation and temperature) is downscaled and bias adjusted, using dynamical and/or statistical approaches and subsequently used to force hydrological models (e.g. Olsson *et al.* 2016). In the present study, we adopt this approach for assessing the climate change impacts on solute transport, using the HYDRUS-1D (Šimůnek *et al.* 2016) as impact model. During the last decade, HYDRUS-1D has been widely used to simulate water flow and solute movement of different hypothetical and experimental problems with and without crops under different boundary conditions (e.g. Harman *et al.* 2011, Sutanto *et al.* 2012, Tafteh and Sepaskhah 2012, Wang *et al.* 2015, Dash *et al.* 2015, Selim *et al.* 2017).

In view of the above, the main goal of the present study is to investigate the effect of climate change on the movement of a conservative non-adsorbing solute in three different soil types cultivated by wheat in three different regions in Sweden. We believe that our study will lead to better understanding of the mechanism of solute dynamics through soil matrix under projected future climate and under the indirect effect of root water uptake. In addition, it will contribute towards a more complete picture of soil and groundwater sustainability in Sweden and other countries with similar conditions.

## Materials and methods

### Site descriptions

Three locations in Sweden were selected (Fig. 1): Malmö (55° 34'17"N, 13°4'24"E), Norrköping (58°34'58"N, 16°8'49"E) and Petisträsk (64°34'1"N, 19°41'54"E) (the exact coordinates refer to the location of existing meteorological stations run by Swedish Meteorological and Hydrological Institute, SMHI). These locations were selected since they represent typical climate conditions for southern, middle (both with humid continental climate with cool summers) and northern (boreal climate) Sweden, respectively. At each site, three different soil



**Figure 1.** Locations of the three sites (from south to north): Malmö, Norrköping and Petisträsk, and the variation of  $P$  and  $PET$  between March and September.

profiles were considered. These profiles are three actual profiles situated close to Malmö. At each site the soil properties were measured every 0.1 m for the first meter and then every 0.5 m. The dominant soil layers were identified and the average soil properties were calculated for each layer. The soil types are referred to as sand, loam and clay according to FAO (2006) are presented in Table 1. Even though the profiles are actual profiles in southern Sweden, they represent typical agricultural soil types found in Sweden (and Northern Europe). The same profiles have also been used in previous studies (Persson and Saifadeen 2016, Selim *et al.* 2017).

## Meteorological data

### Historical observations

All meteorological data were collected by SMHI. Rain gauges used are of weighing type with a volume resolution of 0.1 mm (GEONOR A/S, Oslo, Norway). The original time resolution was 15 min, but in the present study 30 min accumulations were used. This type of rain gauges were installed in a national network in 1996. Available for the present study was a 20-year historical period (1996–2015) that was used as a climatological reference. The observations are subjected to careful quality control before being accepted in the SMHI data base and additional verification was performed during this study.

Potential evapotranspiration calculated using the Penman–Monteith equation (Allen *et al.* 1998) from meteorological measurements were also available for the stations on a monthly time step. The seasonal variation of precipitation (P) and potential evapotranspiration (PET) are similar for the three locations, but with higher PET in the south (especially in spring), reflecting higher temperatures (see Fig. 1).

### Future projections

Future projections of precipitation were available from a limited ensemble of climate model simulations. Two GCMs were used – EC-Earth (Hazeleger *et al.* 2010) and CNRM (Voldoire *et al.* 2013) – each forced with two emission scenarios, i.e. representative concentration pathways (RCPs; Moss *et al.* 2008). The EC-Earth model was forced with RCP2.6 and RCP4.5, representing low and intermediate future emissions of greenhouse gases, respectively, whereas CNRM was forced with RCP4.5 and RCP8.5, where the latter represents high future emissions. We did this selection in order to cover a wide range of possible future climates covering the uncertainties coming from both the GCM and from

the RCP. With the same RCP for both models, we would cover a smaller ‘RCP interval’. As RCP4.5 is considered a ‘medium scenario’, we included two simulations with this RCP. In the following, these combinations of GCMs and RCPs are called EC2.6, EC4.5, CNRM4.5 and CNRM8.5, respectively. These four future projections were dynamically downscaled to a spatial resolution of 11 km and temporal resolution of 30 min by the regional climate model (RCM) RCA4 (Kjellström *et al.* 2016). This resolution is among the higher in RCM projections, which often have a spatial resolution of 25–50 km and rarely an output time step below 1 day. The high resolution is expected to benefit in particular precipitation considering its extreme variability in both time and space.

It is well known that meteorological variables in general and precipitation in particular simulated by climate models are biased. If using the model output directly for subsequent modelling of, for example, hydrological impacts this bias may, at worst, lead to unrealistic results and erroneous conclusions (e.g. Yang *et al.* 2010). Therefore bias adjustment is a key component of the state-of-the-art modelling scheme mentioned in the introduction and it has evolved into a research field of its own (e.g. Maraun *et al.* 2015).

A way to ‘escape’ the issue of climate model bias is to employ the concept of delta change (DC; e.g. Hay *et al.* 2000). In DC, the climate model results are not used directly in the impact modelling but historical observations are statistically modified in order to reflect expected future changes (e.g. by increasing daily precipitation values by a certain percentage) and then these adjusted observations are used to represent future climate. Thus, no assessment is made of the climate model bias, i.e. to which degree the climate models can reproduce observations in a historical reference period, under the assumption that the accuracy of future changes is independent on historical agreement. This may be justified by the existence of climate variability as a key source of bias, i.e. the existence of bias does not necessarily imply that the climate model is inaccurate but rather that the simulation happens to be out-of-phase with low-frequency climate oscillations (e.g. Willems *et al.* 2012).

Delta change is commonly applied on a monthly time scale (e.g. Veijalainen *et al.* 2010). Thus, for each calendar month (e.g. May) a relative scaling factor (or DC factor) is estimated by dividing the May average value for a future time period in a climate projection with the May average in the same projection’s historical reference period. Then, this DC factor is applied to all May values in historical observations to produce a future realisation. When applied to precipitation this basic DC concept has some drawbacks, mainly that (i) the same adjustment is done for average values and extremes and (ii) changes in rainfall frequency (i.e. more or less wet time steps) are not considered.

Olsson *et al.* (2012) developed a DC version which uses high-resolution (sub-hourly) RCM results to overcome the above limitations. First of all, the DC factors are intensity-dependent, i.e. low and high precipitation intensities are adjusted separately. This makes it possible to reproduce rather complex future changes, such as lower summer totals but higher summer extremes, which are commonly found in

**Table 1.** Soil properties, soil texture according to FAO (2006).

| Soil type | Depth (cm) | Sand (%) | Silt (%) | Clay (%) | Bulk density (g/cm <sup>3</sup> ) |
|-----------|------------|----------|----------|----------|-----------------------------------|
| Sand      | 0–20       | 80       | 16.5     | 3.5      | 1.53                              |
|           | 20–45      | 78.8     | 18.3     | 2.9      | 1.55                              |
|           | 45–70      | 84.3     | 11.8     | 3.9      | 1.55                              |
|           | >70        | 93.4     | 4.8      | 1.8      | 1.56                              |
| Loam      | 0–20       | 68.0     | 27.2     | 4.8      | 1.48                              |
|           | 20–150     | 58.2     | 33.0     | 8.9      | 1.48                              |
|           | >150       | 40.5     | 44.6     | 14.9     | 1.65                              |
| Clay      | 0–120      | 59.0     | 25.6     | 15.4     | 1.45                              |
|           | 120–150    | 36.9     | 32.8     | 30.3     | 1.50                              |
|           | >150       | 35.3     | 36.5     | 28.2     | 1.60                              |

climate projections (e.g. Olsson *et al.* 2009). Further, future changes in rainfall frequency may be realized through a procedure in which well-selected observed precipitation events are either removed or copied. See Olsson *et al.* (2012) for more details about the DC procedure.

In the DC application, three 30-year time slices were used for estimating future changes in rainfall statistics (to be transferred onto the historical time series) from the climate projections. In climate research, 30-year periods are common practice in order to get robust statistics with respect to future changes. The historical reference period (1986–2015) includes the 20-year period of the available observations, i.e. 1996–2015. It should be noted that the DC method used is designed to work with data of essentially arbitrary length (although the longer the better). Thus, the fact that the DC factors calculated using 30-year periods are applied to a 20-year periods of historical data is not an inconsistency, but fully in line with the methodology (see e.g. Olsson *et al.* 2012). Two future periods were used, one representing the middle of the current century (2031–2060) and one representing the end of the century (2071–2100). The relative changes between the reference period and the two future periods in all four RCM-projections were thus estimated and applied to the historical period, generating a total of eight future realizations of the precipitation at each site.

For running the solute transport model used we also need input of potential evapotranspiration. This variable is normally very uncertain in GCMs, even more uncertain than precipitation (see, e.g. Kay and Davies 2008). Attempts of using direct output led to unrealistic values (unrealistically high or low values and a very high variability). Instead, we used an ensemble average of nine GCMs to produce more robust estimates of monthly averaged potential evapotranspiration for each emission scenario (see Sjökvist *et al.* 2015). By comparing with monthly averaged evapotranspiration calculated by the same models for the historical period, DC factors for each emission scenario and future period were calculated. These DC factors were then applied to the evapotranspiration data series for the historical period to produce time series for the future scenarios. This gave stable and realistic evapotranspiration values, however, it also led to the values for the RCP4.5 scenario being identical for both GCMs.

## HYDRUS model

### System description

The domain geometry used to simulate solute transport under point source pollutant was one-dimensional (1D) and 2.50 m deep. The domain depth represents the typical depth of the ground water table in agricultural lands in Sweden. In total, 101 1D elements were used to discretize the simulation domain. The simulation domain was divided into sub-regions (four sub-regions in case of sand soil and three in case of loam and clay soils) to capture the variation in soil hydraulic properties throughout the simulation domain. Simulations of solute transport penetration were conducted yearly, the simulation period was 5000 h long, representing the period between 1 March and 25 September. The input

time step of precipitation and evaporation was 0.5 h. This period represents approximately the growing season. By choosing this period we avoid problems with periods with below freezing temperatures and frozen soils.

### Soil hydraulic parameters and solute parameters

Soil hydraulic parameters (Van Genuchten 1980) were estimated using the ROSETTA software package (Schaap *et al.* 2001), incorporated within HYDRUS-1D, using measured bulk density and percentages of sand, silt and clay (Table 2). Soil water hysteresis was considered, it was assumed that the  $\alpha$  value for the drying curve was half the value of the wetting curve (e.g. Kool and Parker 1987, Selim *et al.* 2017). Solute parameters required during the present work were longitudinal dispersivity, molecular diffusion and adsorption isotherm coefficient. Longitudinal dispersivity was set to one-tenth of the profile depth (e.g. Anderson 1984, Cote *et al.* 2001). Molecular diffusion and adsorption were neglected during simulation.

### Initial conditions

Based on a water table located 2.50 m below the soil surface, initial pressure head was assumed to vary linearly between 0 at the bottom edge of simulation domain to  $-2.50$  at the surface. The simulation domain was assumed to be initially free of pollutants except the top 5 cm, where 100 g of a non-absorbing conservative solute was uniformly distributed at the start of each modelling year (1 March). This scheme was selected as we wanted the solutes to be spread at the same circumstances every year and subsequent solute movement being only driven by the precipitation falling after the start of the simulation period.

### Boundary conditions

As the water table is located 2.50 m below the soil surface, constant pressure head boundary conditions (BC) with a pressure head equal to zero was set at the lower edge of the simulation domain. Atmospheric BC, permitting for crop evapotranspiration (ET<sub>c</sub>), was set at the upper edge of the simulation domain. Spring wheat, which is among the most important agricultural crops in Sweden, was assumed to be grown during the period from the 29th of March to 5th of August in all simulation scenarios. In order to estimate ET<sub>c</sub>, the CROPWAT model (FAO 2012) was used to estimate daily reference crop evapotranspiration (ET<sub>o</sub>) based on the meteorological data. The collected meteorological data from

**Table 2.** Soil hydraulic properties, parameters of the Van Genuchten (1980) model.

| Soil type | Depth (cm) | $\theta_r$ | $\theta_s$ | $A$ (cm <sup>-1</sup> ) | $n$   | $K_s$ (cm/h) | $l$ |
|-----------|------------|------------|------------|-------------------------|-------|--------------|-----|
| Sand      | 0–20       | 0.0388     | 0.372      | 0.0437                  | 1.818 | 5.011        | 0.5 |
|           | 20–45      | 0.0369     | 0.3639     | 0.0457                  | 1.769 | 4.374        | 0.5 |
|           | 45–70      | 0.043      | 0.3709     | 0.402                   | 2.081 | 7.01         | 0.5 |
|           | >70        | 0.0492     | 0.3677     | 0.034                   | 3.255 | 24.16        | 0.5 |
| Loam      | 0–20       | 0.0341     | 0.3714     | 0.0383                  | 1.476 | 2.70         | 0.5 |
|           | 20–150     | 0.0382     | 0.3683     | 0.024                   | 1.432 | 1.53         | 0.5 |
|           | >150       | 0.0444     | 0.3334     | 0.0141                  | 1.406 | 0.32         | 0.5 |
| Clay      | 0–120      | 0.0518     | 0.3974     | 0.021                   | 1.438 | 1.27         | 0.5 |
|           | 120–150    | 0.0749     | 0.4078     | 0.0129                  | 1.407 | 0.26         | 0.5 |
|           | >150       | 0.0682     | 0.3773     | 0.0127                  | 1.384 | 0.16         | 0.5 |

Malmö, Norrköping and Petisträsk during the 20-year period from 1996 to 2015 was averaged on daily basis and used as input data for the CROPWAT model. Then, the calculated  $ET_o$  was multiplied by the crop coefficient for spring wheat to estimate daily  $ET_c$ . Each growing stage (i.e. initial, development, mid and late) was multiplied by the corresponding crop coefficient,  $K_c$  (Allen *et al.* 1998). The calculated  $ET_c$  was used during the simulation of the historical period. By using the output of GCMs forced by different RCPs, the change in  $ET_c$  was calculated for each of the future climate projections. Daily values of  $ET_c$  were downscaled to a 0.5-h time step by assuming a sinusoidal variation between sunrise and sunset and evapotranspiration was neglected during the night. The HYDRUS-1D model do not use  $ET_c$  as input data, it instead considers evaporation ( $E$ ) and transpiration ( $T$ ) rates. To separate the calculated  $ET_c$  to  $E$  and  $T$  rates, the Belmans *et al.* (1983) equation for calculating  $E$  was used. The evaporation rate was estimated based on the leaf area index (LAI) and the extinction coefficient for solar radiation of 0.39 (Ritchie 1972). The WOFOST model (Boogaard *et al.* 1998) was used to calculate LAI for spring wheat during its different growth stages. For more details about calculation of  $ET_c$  and how to separate it into  $E$  and  $T$ , see Selim *et al.* (2017). The evaporation rate was set equal to  $ET_o$  during the period before and after the spring wheat growing date. During simulations, water ponding was allowed at the surface while surface runoff was neglected. Zero concentration gradient and concentration flux boundary conditions were assigned at the bottom and the top edges of simulation domain, respectively.

### Root growth and root water uptake parameters

Root growth is determined based on the assumption that half of the rooting depth will be reached at the middle of the growing season (Šimůnek *et al.* 2008). In all simulation scenarios, the initial and maximum spring wheat rooting depths were set equal to 0.07 and 1.20 m, respectively (Zhou *et al.* 2012). Based on sowing and harvesting dates, the initial root growth and harvest times were assigned. To consider the effect of water deficit on root water uptake, the Feddes *et al.* (1978) model was used. This model is parameterized by four critical values of the water pressure head,  $h_3 < h_2 < h_{opt} < h_o$  describing plant stress due to dry and wet soil conditions:

$$\alpha(h) = \begin{cases} \frac{h-h_3}{h_2-h_3} & h_2 > h > h_3 \\ 1 & h_{opt} > h > h_2 \\ \frac{h-h_o}{h_{opt}-h_o} & h_o > h > h_{opt} \\ 0 & h \geq h_o \text{ or } h \leq h_3 \end{cases} \quad (1)$$

where  $h$  is the pressure head,  $h_o$  is the pressure head below which roots start to extract water from the soil,  $h_{opt}$  is the pressure head below which roots extract water at the maximum possible rate,  $h_2$  is the limiting pressure head below which roots can no longer extract water at the maximum rate (and is a function of evaporative demand) and  $h_3$  is the pressure head below which root water uptake ceases (the wilting point). In the HYDRUS model, two values,  $h_{2H}$  and  $h_{2L}$ , related to higher and lower potential transpiration ( $r_{2H}$  and  $r_{2L}$ ), respectively, should be set for  $h_2$ .

During simulation the following parameters were used;  $h_o = 0$ ,  $h_{opt} = -1$  cm,  $h_{2H} = -500$  cm,  $h_{2L} = -900$  cm,  $h_3 = -16,000$ ,  $r_{2H} = 0.50$  cm/h and  $r_{2L} = 0.1$  cm/h. Salinity stress reduction effects were ignored during the simulations.

### Solute transport for different climate scenarios

The solute distribution at the end of the 5000-h simulation period was estimated using HYDRUS-1D. In total 1620 simulations of solute displacement were conducted (20 years  $\times$  9 periods (1 historical and 8 future)  $\times$  3 soil types  $\times$  3 sites). In order to quantify the solute transport and to facilitate the comparison between different simulations, two variables to describe the solute displacement were calculated. These were; (i) the depth from the surface to the centre of mass of the solute,  $z_{COM}$  and the deepest depth where the concentration exceeded a given limit concentration,  $z_{LC}$  (in our case the limit was arbitrarily set to 0.2 g/L). These parameters represent the average and deepest solute transport, respectively. In order to investigate the significance of the difference between the  $z_{COM}$  and  $z_{LC}$  calculated using different rainfall data, the paired Student's  $t$ -test was performed.

## Results and discussion

### Precipitation and evapotranspiration for different climate projections

A summary of the rainfall for the historical and future periods can be found in Table 3. The  $t$ -test showed that all changes in precipitation were significant at the  $p = 0.05$  level, except EC2.6 at mid-century and EC4.5 at end-century in Malmö and Norrköping. Most projections predict an increase in precipitation to mid-century and a further increase to end-century. The only significant decrease in precipitation was predicted with EC2.6 in Malmö and Norrköping.

Table 4 shows the future changes in some key precipitation characteristics during the studied period (March–September)

**Table 3.** Rainfall volumes (in mm) for different locations, periods and scenarios. The values are the average for the 5000-h periods studied each year during a 20-year period.

| Source            | Historical<br>1996–2015 | Mid-century<br>2031–2050 | End-century<br>2071–2090 |
|-------------------|-------------------------|--------------------------|--------------------------|
| <i>Malmö</i>      |                         |                          |                          |
| Measured          | 362                     |                          |                          |
| EC2.6             |                         | 327                      | 369                      |
| EC4.5             |                         | 366                      | 352                      |
| CNRM4.5           |                         | 410                      | 488                      |
| CNRM8.5           |                         | 438                      | 471                      |
| <i>Norrköping</i> |                         |                          |                          |
| Measured          | 346                     |                          |                          |
| EC2.6             |                         | 332                      | 350                      |
| EC4.5             |                         | 354                      | 372                      |
| CNRM4.5           |                         | 391                      | 406                      |
| CNRM8.5           |                         | 383                      | 446                      |
| <i>Petisträsk</i> |                         |                          |                          |
| Measured          | 349                     |                          |                          |
| EC2.6             |                         | 356                      | 374                      |
| EC4.5             |                         | 414                      | 463                      |
| CNRM4.5           |                         | 385                      | 431                      |
| CNRM8.5           |                         | 369                      | 449                      |

**Table 4.** Future relative changes (%) in average, maximum and frequency of precipitation in the different locations and for different climate projections. Positive change indicates increasing values compared to the historical data.

| Modell            | RCP | Mid-century |         |           | End-century |         |           |
|-------------------|-----|-------------|---------|-----------|-------------|---------|-----------|
|                   |     | Average     | Maximum | Frequency | Average     | Maximum | Frequency |
| <i>Malmö</i>      |     |             |         |           |             |         |           |
| EC-Earth          | 2.6 | −6.0        | 6.1     | −7.4      | 5.5         | 2.8     | 1.5       |
|                   | 4.5 | −0.2        | 6.5     | −4.3      | −1.4        | −0.6    | −3.4      |
| CNRM              | 4.5 | 13.7        | 7.1     | 10.4      | 36.2        | 9.4     | 26.7      |
|                   | 8.5 | 23.3        | 3.0     | 18.0      | 33.1        | 31.7    | 18.7      |
| <i>Norrköping</i> |     |             |         |           |             |         |           |
| EC-Earth          | 2.6 | 3.6         | −1.0    | −1.6      | 3.8         | 0.6     | −0.3      |
|                   | 4.5 | 0.4         | 2.2     | −2.1      | 8.6         | 9.5     | 0.6       |
| CNRM              | 4.5 | 11.4        | 16.1    | 10.0      | 17.7        | 7.0     | 15.2      |
|                   | 8.5 | 11.0        | 2.8     | 12.5      | 33.7        | 18.0    | 19.5      |
| <i>Petisträsk</i> |     |             |         |           |             |         |           |
| EC-Earth          | 2.6 | 6.7         | 3.2     | 5.9       | 10.9        | 9.8     | 6.5       |
|                   | 4.5 | 15.6        | 15.2    | 7.6       | 34.4        | 17.2    | 22.5      |
| CNRM              | 4.5 | 9.7         | −10.9   | 11.9      | 26.5        | 3.6     | 23.1      |
|                   | 8.5 | 9.0         | −1.8    | 10.4      | 40.3        | 1.1     | 35.5      |

as estimated from the climate projections. The future changes in both Malmö and Norrköping are consistently very small in the EC-Earth projections, whereas all metrics (average, maximum and frequency) exhibit a distinct increase in Petisträsk, most pronounced for RCP4.5 at end-century. In the CNRM projections there is a consistent and distinct increase in both average precipitation and precipitation frequency, whereas the increase in maximum precipitation is markedly lower and even negative (Petisträsk, mid-century).

In Malmö and Norrköping there is clearly a larger difference between the results from different GCMs than from different RCPs. The same tendency can be seen in Petisträsk, although less clear. It should be emphasized that the ensemble of projections spans a large range of different possible future changes, making it well suited for investigating possible impacts on solute transport.

The potential evapotranspiration (Table 5) also showed an increasing trend with time for all projections and locations, generally with higher increases in northern Sweden (Petisträsk). The total evapotranspiration was still clearly larger in Malmö than in Petisträsk, but the difference decreased, from around 40% in the historical period to around 30% at

**Table 5.** Potential evaporation volumes (in mm) for different locations, periods and scenarios. The values are the average for the 5000-h periods studied each year during a 20-year period.

| Source            | Historical<br>1996–2015 | Mid-century<br>2031–2050 | End-century<br>2071–2090 |
|-------------------|-------------------------|--------------------------|--------------------------|
| <i>Malmö</i>      |                         |                          |                          |
| Measured          | 610                     |                          |                          |
| EC2.6             |                         | 634                      | 635                      |
| EC4.5             |                         | 656                      | 659                      |
| CNRM4.5           |                         | 656                      | 659                      |
| CNRM8.5           |                         | 665                      | 714                      |
| <i>Norrköping</i> |                         |                          |                          |
| Measured          | 577                     |                          |                          |
| EC2.6             |                         | 606                      | 609                      |
| EC4.5             |                         | 623                      | 632                      |
| CNRM4.5           |                         | 623                      | 632                      |
| CNRM8.5           |                         | 635                      | 678                      |
| <i>Petisträsk</i> |                         |                          |                          |
| Measured          | 433                     |                          |                          |
| EC2.6             |                         | 472                      | 475                      |
| EC4.5             |                         | 503                      | 507                      |
| CNRM4.5           |                         | 503                      | 507                      |
| CNRM8.5           |                         | 509                      | 541                      |

late-century. The net change in the difference between precipitation and potential evapotranspiration decreased in 75% of the future projections.

### Solute transport for different climate projections

Results in terms of  $z_{\text{COM}}$  and  $z_{\text{LC}}$  are presented as averages and standard deviation (SD) for each scenario, soil type and location are presented in Tables 6–11. In the tables, values indicating a significantly increased risk for groundwater contamination (or, equivalently, a higher solute transport

**Table 6.** The average depth from the surface to the centre of mass of the solute,  $z_{\text{COM}}$  (in m) and the standard deviation (SD) for clay for different locations and time periods, and for different scenarios. Values in italics represent a significantly lowered risk for groundwater contamination and values in bold represent a significantly increased risk for groundwater contamination.

| Source of input   | Historical<br>1996–2015 |       | Mid-century<br>2031–2050 |       | End-century<br>2071–2090 |       |
|-------------------|-------------------------|-------|--------------------------|-------|--------------------------|-------|
|                   | Average                 | SD    | Average                  | SD    | Average                  | SD    |
| <i>Malmö</i>      |                         |       |                          |       |                          |       |
| Measured          | 0.360                   | 0.150 |                          |       |                          |       |
| EC2.6             |                         |       | 0.327*                   | 0.099 | 0.361                    | 0.141 |
| EC4.5             |                         |       | 0.348*                   | 0.150 | 0.332*                   | 0.106 |
| CNRM4.5           |                         |       | <b>0.395**</b>           | 0.166 | <b>0.502**</b>           | 0.263 |
| CNRM8.5           |                         |       | <b>0.424**</b>           | 0.187 | <b>0.441**</b>           | 0.216 |
| <i>Norrköping</i> |                         |       |                          |       |                          |       |
| Measured          | 0.315                   | 0.068 |                          |       |                          |       |
| EC2.6             |                         |       | 0.329                    | 0.081 | 0.325                    | 0.074 |
| EC4.5             |                         |       | 0.309                    | 0.072 | 0.334                    | 0.082 |
| CNRM4.5           |                         |       | <b>0.350*</b>            | 0.094 | 0.342                    | 0.084 |
| CNRM8.5           |                         |       | 0.328                    | 0.080 | <b>0.367*</b>            | 0.096 |
| <i>Petisträsk</i> |                         |       |                          |       |                          |       |
| Measured          | 0.445                   | 0.144 |                          |       |                          |       |
| EC2.6             |                         |       | 0.429                    | 0.141 | 0.458                    | 0.160 |
| EC4.5             |                         |       | <b>0.499*</b>            | 0.181 | <b>0.581**</b>           | 0.198 |
| CNRM4.5           |                         |       | 0.443                    | 0.147 | <b>0.516*</b>            | 0.175 |
| CNRM8.5           |                         |       | 0.426                    | 0.129 | <b>0.512*</b>            | 0.163 |

\*significant at the 0.05 level; \*\*significant at the 0.01 level

**Table 7.** The average depth from the surface to the limit concentration of the solute,  $z_{\text{LC}}$  (in m) and the standard deviation (SD) for clay for different locations and time periods, and different scenarios. Values in italics represent a significantly lowered risk for groundwater contamination and values in bold represent a significantly increased risk for groundwater contamination.

| Source of input   | Historical<br>1996–2015 |       | Mid-century<br>2031–2050 |       | End-century<br>2071–2090 |       |
|-------------------|-------------------------|-------|--------------------------|-------|--------------------------|-------|
|                   | Average                 | SD    | Average                  | SD    | Average                  | SD    |
| <i>Malmö</i>      |                         |       |                          |       |                          |       |
| Measured          | 0.778                   | 0.145 |                          |       |                          |       |
| EC2.6             |                         |       | 0.745*                   | 0.120 | 0.788                    | 0.140 |
| EC4.5             |                         |       | 0.767*                   | 0.146 | 0.748**                  | 0.131 |
| CNRM4.5           |                         |       | <b>0.804**</b>           | 0.133 | <b>0.904**</b>           | 0.164 |
| CNRM8.5           |                         |       | <b>0.853**</b>           | 0.167 | <b>0.855**</b>           | 0.160 |
| <i>Norrköping</i> |                         |       |                          |       |                          |       |
| Measured          | 0.775                   | 0.077 |                          |       |                          |       |
| EC2.6             |                         |       | 0.758                    | 0.062 | 0.760*                   | 0.064 |
| EC4.5             |                         |       | 0.761                    | 0.075 | 0.775                    | 0.069 |
| CNRM4.5           |                         |       | <b>0.806*</b>            | 0.086 | <b>0.803**</b>           | 0.073 |
| CNRM8.5           |                         |       | 0.772                    | 0.070 | <b>0.841**</b>           | 0.082 |
| <i>Petisträsk</i> |                         |       |                          |       |                          |       |
| Measured          | 0.851                   | 0.128 |                          |       |                          |       |
| EC2.6             |                         |       | 0.825                    | 0.129 | 0.851                    | 0.140 |
| EC4.5             |                         |       | 0.881                    | 0.143 | <b>0.955**</b>           | 0.137 |
| CNRM4.5           |                         |       | 0.830                    | 0.130 | <b>0.894*</b>            | 0.122 |
| CNRM8.5           |                         |       | 0.817*                   | 0.123 | <b>0.896**</b>           | 0.110 |

\*significant at the 0.05 level; \*\*significant at the 0.01 level.

**Table 8.** The average depth from the surface to the centre of mass of the solute,  $z_{COM}$  (in m) and the standard deviation (SD) for loam for different locations and time periods, and different scenarios. Values in italics represent a significantly lowered risk for groundwater contamination and values in bold represent a significantly increased risk for groundwater contamination.

| Source of input   | Historical<br>1996–2015 |       | Mid-century<br>2031–2050 |       | End-century<br>2071–2090 |       |
|-------------------|-------------------------|-------|--------------------------|-------|--------------------------|-------|
|                   | Average                 | SD    | Average                  | SD    | Average                  | SD    |
| <i>Malmö</i>      |                         |       |                          |       |                          |       |
| Measured          | 0.381                   | 0.170 |                          |       |                          |       |
| EC2.6             |                         |       | <i>0.346*</i>            | 0.116 | 0.383                    | 0.157 |
| EC4.5             |                         |       | 0.371                    | 0.170 | <i>0.350*</i>            | 0.124 |
| CNRM4.5           |                         |       | <b>0.426**</b>           | 0.185 | <b>0.555**</b>           | 0.294 |
| CNRM8.5           |                         |       | <b>0.460**</b>           | 0.214 | <b>0.483**</b>           | 0.257 |
| <i>Norrköping</i> |                         |       |                          |       |                          |       |
| Measured          | 0.339                   | 0.077 |                          |       |                          |       |
| EC2.6             |                         |       | 0.345                    | 0.096 | 0.344                    | 0.086 |
| EC4.5             |                         |       | 0.326                    | 0.085 | 0.366                    | 0.094 |
| CNRM4.5           |                         |       | <b>0.387*</b>            | 0.109 | 0.363                    | 0.096 |
| CNRM8.5           |                         |       | 0.352                    | 0.091 | <b>0.396*</b>            | 0.114 |
| <i>Petisträsk</i> |                         |       |                          |       |                          |       |
| Measured          | 0.480                   | 0.165 |                          |       |                          |       |
| EC2.6             |                         |       | 0.463                    | 0.163 | 0.503                    | 0.179 |
| EC4.5             |                         |       | <b>0.546*</b>            | 0.208 | <b>0.647**</b>           | 0.231 |
| CNRM4.5           |                         |       | 0.482                    | 0.167 | <b>0.568**</b>           | 0.200 |
| CNRM8.5           |                         |       | 0.462                    | 0.145 | <b>0.567**</b>           | 0.186 |

\*significant at the 0.05 level; \*\*significant at the 0.01 level.

**Table 9.** The average depth from the surface to the limit concentration of the solute,  $z_{LC}$  (in m) and the standard deviation (SD) for loam for different locations and time periods, and different scenarios. Values in italics represent a significantly lowered risk for groundwater contamination and values in bold represent a significantly increased risk for groundwater contamination.

| Source of input   | Historical<br>1996–2015 |       | Mid-century<br>2031–2050 |       | End-century<br>2071–2090 |       |
|-------------------|-------------------------|-------|--------------------------|-------|--------------------------|-------|
|                   | Average                 | SD    | Average                  | SD    | Average                  | SD    |
| <i>Malmö</i>      |                         |       |                          |       |                          |       |
| Measured          | 0.851                   | 0.153 |                          |       |                          |       |
| EC2.6             |                         |       | <i>0.828*</i>            | 0.136 | 0.861                    | 0.151 |
| EC4.5             |                         |       | 0.838                    | 0.154 | <i>0.829*</i>            | 0.138 |
| CNRM4.5           |                         |       | <b>0.882**</b>           | 0.160 | <b>1.001**</b>           | 0.208 |
| CNRM8.5           |                         |       | <b>0.921**</b>           | 0.179 | <b>0.932**</b>           | 0.175 |
| <i>Norrköping</i> |                         |       |                          |       |                          |       |
| Measured          | 0.835                   | 0.087 |                          |       |                          |       |
| EC2.6             |                         |       | 0.824                    | 0.069 | 0.829                    | 0.071 |
| EC4.5             |                         |       | <i>0.812**</i>           | 0.078 | 0.847                    | 0.077 |
| CNRM4.5           |                         |       | <b>0.888**</b>           | 0.095 | <b>0.881**</b>           | 0.077 |
| CNRM8.5           |                         |       | 0.839                    | 0.078 | <b>0.921**</b>           | 0.083 |
| <i>Petisträsk</i> |                         |       |                          |       |                          |       |
| Measured          | 0.926                   | 0.149 |                          |       |                          |       |
| EC2.6             |                         |       | 0.910                    | 0.152 | 0.958                    | 0.166 |
| EC4.5             |                         |       | 0.971                    | 0.163 | <b>1.031**</b>           | 0.144 |
| CNRM4.5           |                         |       | 0.917                    | 0.154 | <b>0.998**</b>           | 0.161 |
| CNRM8.5           |                         |       | 0.903                    | 0.138 | <b>0.998**</b>           | 0.147 |

\*significant at the 0.05 level; \*\*significant at the 0.01 level.

velocity) are in bold while values indicating a significantly decreased risk for groundwater contamination are in italics.

As the soil types are different in terms of soil texture, soil layering and initial water content profiles, different soil types should not be compared, but rather the same soil type at the different sites should be compared. However, some general differences between the different soil types could be pointed out. Both absolute and relative changes were larger in sand compared to clay, with loam in between. This would indicate that coarse textured soils are more sensitive to changes in precipitation compared to fine textured soils, but one should

**Table 10.** The average depth from the surface to the centre of mass of the solute,  $z_{COM}$  (in m) and the standard deviation (SD) for sand for different locations and time periods, and different scenarios. Values in italics represent a significantly lowered risk for groundwater contamination and values in bold represent a significantly increased risk for groundwater contamination.

| Source of input   | Historical<br>1996–2015 |       | Mid-century<br>2031–2050 |       | End-century<br>2071–2090 |       |
|-------------------|-------------------------|-------|--------------------------|-------|--------------------------|-------|
|                   | Average                 | SD    | Average                  | SD    | Average                  | SD    |
| <i>Malmö</i>      |                         |       |                          |       |                          |       |
| Measured          | 0.675                   | 0.307 |                          |       |                          |       |
| EC2.6             |                         |       | <i>0.623*</i>            | 0.261 | 0.686                    | 0.302 |
| EC4.5             |                         |       | <i>0.645*</i>            | 0.310 | <i>0.618*</i>            | 0.277 |
| CNRM4.5           |                         |       | <b>0.734**</b>           | 0.332 | <b>0.935**</b>           | 0.429 |
| CNRM8.5           |                         |       | <b>0.815**</b>           | 0.354 | <b>0.846**</b>           | 0.385 |
| <i>Norrköping</i> |                         |       |                          |       |                          |       |
| Measured          | 0.609                   | 0.176 |                          |       |                          |       |
| EC2.6             |                         |       | 0.613                    | 0.184 | 0.613                    | 0.155 |
| EC4.5             |                         |       | 0.568                    | 0.154 | 0.638                    | 0.163 |
| CNRM4.5           |                         |       | <b>0.711**</b>           | 0.202 | <b>0.696*</b>            | 0.177 |
| CNRM8.5           |                         |       | 0.625                    | 0.170 | <b>0.769**</b>           | 0.214 |
| <i>Petisträsk</i> |                         |       |                          |       |                          |       |
| Measured          | 0.813                   | 0.314 |                          |       |                          |       |
| EC2.6             |                         |       | 0.799                    | 0.312 | 0.857                    | 0.324 |
| EC4.5             |                         |       | <b>0.939*</b>            | 0.347 | <b>1.101**</b>           | 0.346 |
| CNRM4.5           |                         |       | 0.832                    | 0.319 | <b>0.990**</b>           | 0.333 |
| CNRM8.5           |                         |       | 0.803                    | 0.303 | <b>1.025**</b>           | 0.327 |

\*significant at the 0.05 level; \*\*significant at the 0.01 level.

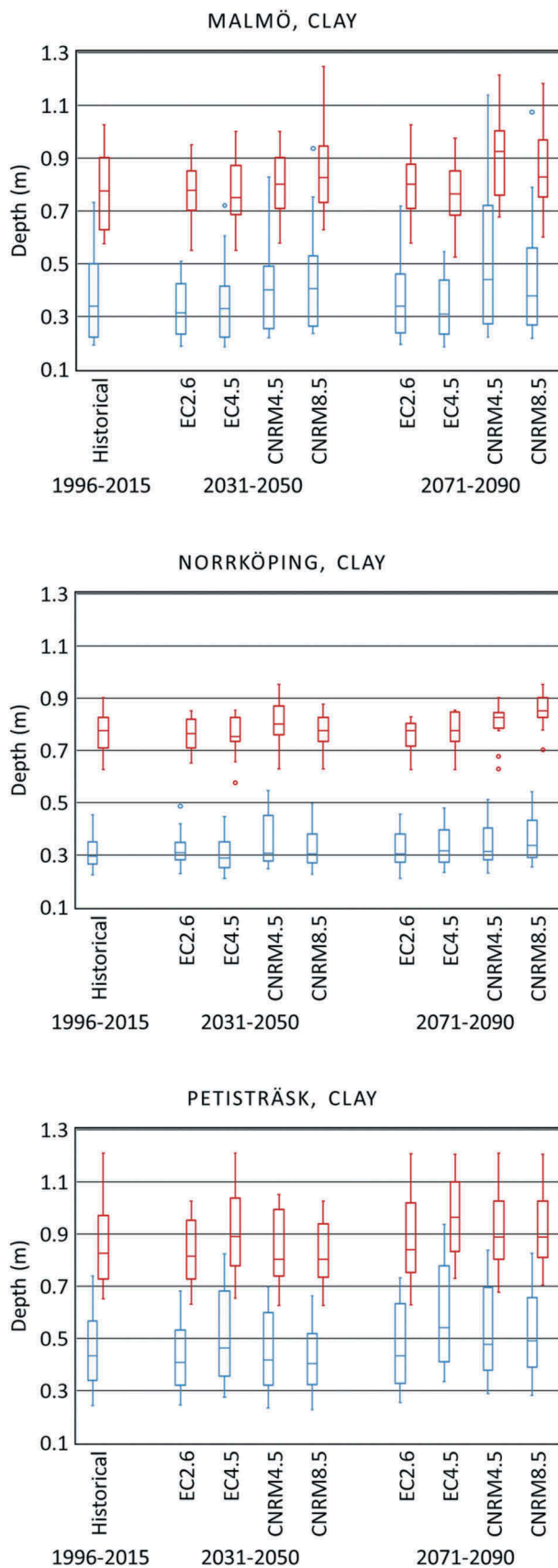
**Table 11.** The average depth from the surface to the limit concentration of the solute,  $z_{LC}$  (in m) and the standard deviation (SD) for sand for different locations and time periods, and different scenarios. Values in italics represent a significantly lowered risk for groundwater contamination and values in bold represent a significantly increased risk for groundwater contamination.

| Source of input   | Historical<br>1996–2015 |       | Mid-century<br>2031–2050 |       | End-century<br>2071–2090 |       |
|-------------------|-------------------------|-------|--------------------------|-------|--------------------------|-------|
|                   | Average                 | SD    | Average                  | SD    | Average                  | SD    |
| <i>Malmö</i>      |                         |       |                          |       |                          |       |
| Measured          | 1.472                   | 0.511 |                          |       |                          |       |
| EC2.6             |                         |       | 1.429                    | 0.480 | <b>1.512*</b>            | 0.509 |
| EC4.5             |                         |       | <i>1.423*</i>            | 0.512 | <i>1.419*</i>            | 0.486 |
| CNRM4.5           |                         |       | <b>1.562**</b>           | 0.495 | <b>1.784**</b>           | 0.537 |
| CNRM8.5           |                         |       | <b>1.656**</b>           | 0.501 | <b>1.705**</b>           | 0.511 |
| <i>Norrköping</i> |                         |       |                          |       |                          |       |
| Measured          | 1.436                   | 0.356 |                          |       |                          |       |
| EC2.6             |                         |       | 1.455                    | 0.331 | 1.416                    | 0.285 |
| EC4.5             |                         |       | 1.320                    | 0.307 | 1.474                    | 0.282 |
| CNRM4.5           |                         |       | 1.551                    | 0.322 | <b>1.555*</b>            | 0.303 |
| CNRM8.5           |                         |       | 1.430                    | 0.293 | <b>1.713**</b>           | 0.300 |
| <i>Petisträsk</i> |                         |       |                          |       |                          |       |
| Measured          | 1.615                   | 0.431 |                          |       |                          |       |
| EC2.6             |                         |       | 1.624                    | 0.436 | 1.689                    | 0.440 |
| EC4.5             |                         |       | <b>1.780*</b>            | 0.450 | <b>1.990**</b>           | 0.419 |
| CNRM4.5           |                         |       | 1.642                    | 0.432 | <b>1.855**</b>           | 0.416 |
| CNRM8.5           |                         |       | 1.609                    | 0.433 | <b>1.910**</b>           | 0.399 |

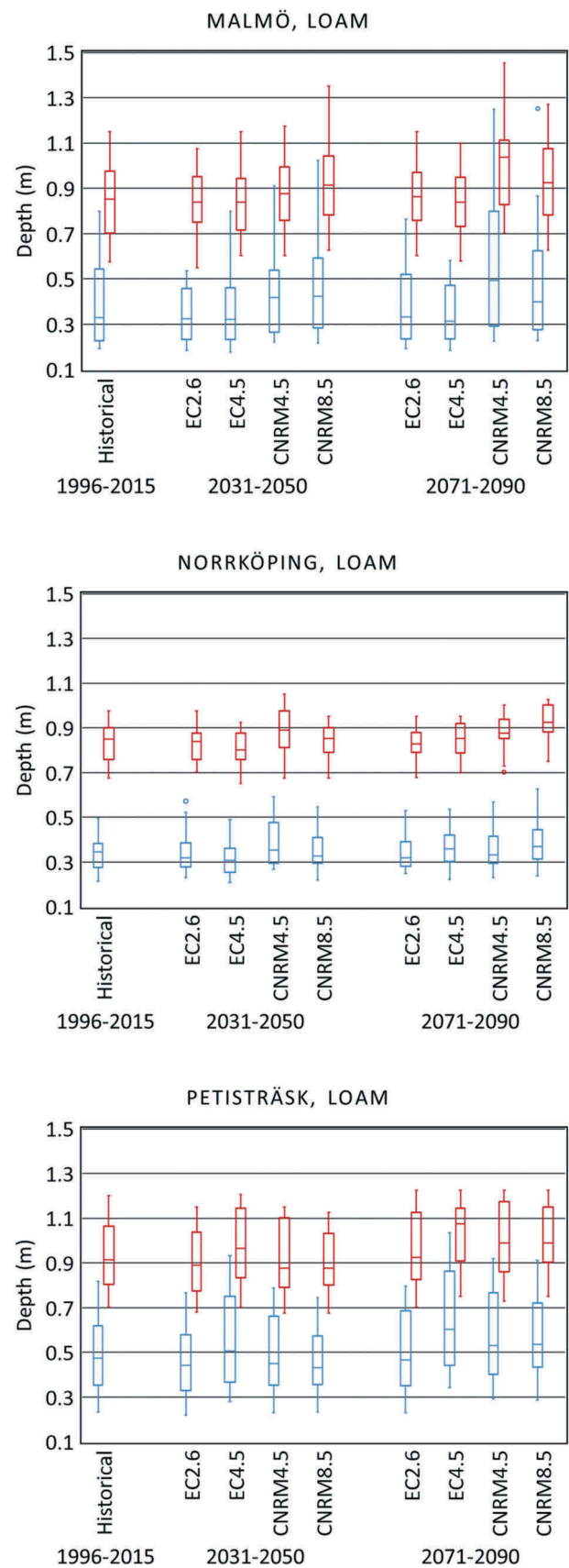
\*significant at the 0.05 level; \*\*significant at the 0.01 level.

bear in mind that the differences were small. In general, both  $z_{COM}$  and  $z_{LC}$  behaved in a similar manner. For clay and loam the absolute changes in  $z_{LC}$  were similar to those for  $z_{COM}$ . For sand, on the other hand, the absolute changes in  $z_{LC}$  were larger than those for  $z_{COM}$ . Again, this implies that in coarse textured soils the groundwater contamination risk would increase more than in fine textured soils for a given increase in precipitation.

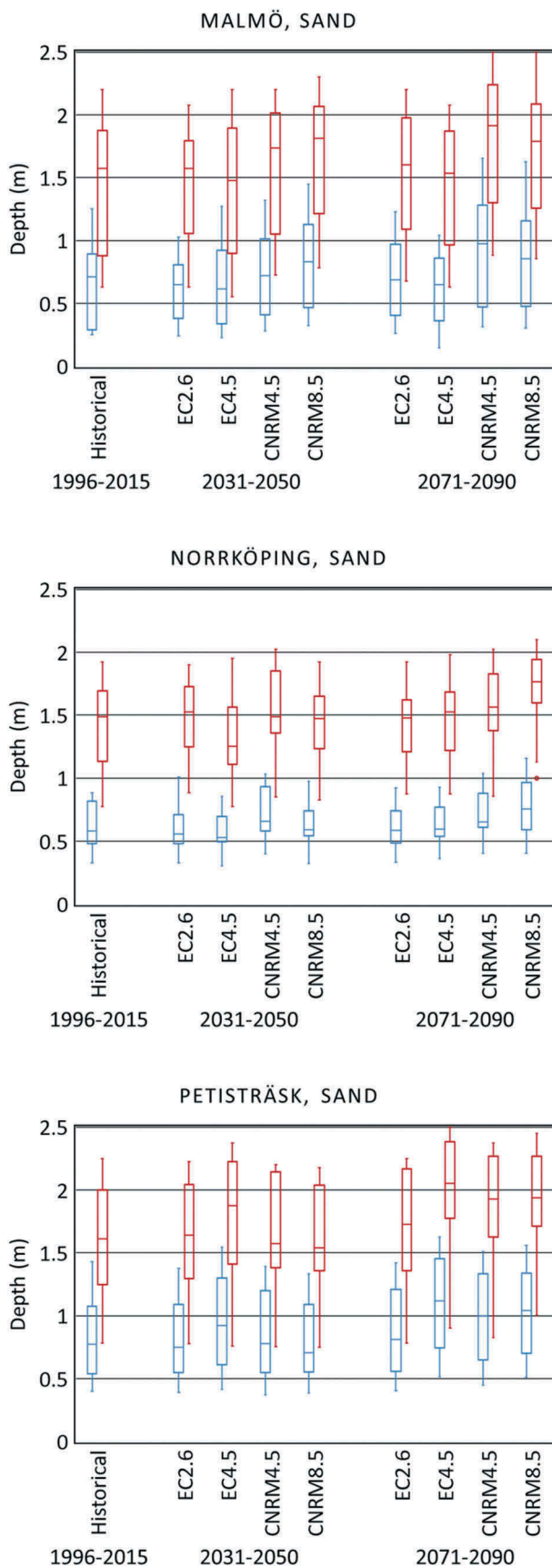
Results are also presented as box and whisker charts in Figs. 2–4 in order to display the variability of the data. From these figures, it can be seen that the variability in  $z_{COM}$  and  $z_{LC}$  is quite large. In general, variability was smaller in



**Figure 2.** Box-and-whisker plots of  $z_{COM}$  (blue) and  $z_{LC}$  (red) for the three sites for clay. The horizontal line within each box shows the median, boundaries of the box indicate the 25th and 75th percentiles, and the whiskers indicate the highest and lowest values of the data series. Outliers are presented as circles.



**Figure 3.** Box-and-whisker plots of  $z_{COM}$  (blue) and  $z_{LC}$  (red) for the three sites for loam. The horizontal line within each box shows the median, boundaries of the box indicate the 25th and 75th percentiles, and the whiskers indicate the highest and lowest values of the data series. Outliers are presented as circles.



**Figure 4.** Box-and-whisker plots of  $z_{COM}$  (blue) and  $z_{LC}$  (red) for the three sites for sand. The horizontal line within each box shows the median, boundaries of the box indicate the 25th and 75th percentiles, and the whiskers indicate the highest and lowest values of the data series. Outliers are presented as circles.

Norrköping, explained by the lower variability in precipitation for different years for this site (the standard deviations of the seasonal precipitation were 95, 44 and 79 mm for Malmö, Norrköping and Petisträsk, respectively). The standard deviation of  $z_{COM}$  was more or less unchanged for mid-century compared to the historical period, but increased for the end-century in all cases except for sand in Petisträsk. For the standard deviation of  $z_{LC}$  a small decrease until mid-century followed by an increase to end-century was found in Malmö, in the other locations the SD was more or less unchanged for mid-century and then decreased for end-century.

Changes in average simulated solute transport depths for different projections compared to the historical period varied substantially, from  $-10\%$  (Malmö, loam, EC2.6, mid-century) to  $+45\%$  (Malmö, loam, CNRM4.5, end-century) for  $z_{COM}$ . It is interesting to compare the changes with the intra-annual variability of  $z_{COM}$ . One way of doing this is to compare the changes with the standard deviations of the  $z_{COM}$  for the historical periods. In all cases the absolute changes were smaller than the SD, however, the highest increases were almost as large as the SD. The changes in  $z_{LC}$  displayed a slightly smaller range compared to  $z_{COM}$ , from  $-8\%$  (Norrköping, sand, EC4.5, mid-century) to  $+23\%$  (Petisträsk, sand, EC4.5, end-century). The increases in  $z_{COM}$  and  $z_{LC}$  are related to increases in precipitation volume, wet fraction and increasing precipitation intensity. These parameters have also previously been shown to increase solute penetration depths (Persson and Saifadeen 2016).

In southern Sweden (Malmö) the CRNM model gave a significantly increasing groundwater contamination risk for both the RCP4.5 and RCP8.5 and both mid and end-century. In northern Sweden (Petisträsk), on the other hand, the CRNM model generally predicted an unchanged risk for mid-century and a significantly increasing groundwater contamination risk for end-century. The EC model generally gave unchanged or a decreasing risk in Malmö and Norrköping, while in Petisträsk results were mixed. Apparently, the generally increasing trends of both precipitation ( $P$ ) and potential evapotranspiration ( $PET$ ) seems to lead to an unchanged or increasing  $z_{COM}$  and  $z_{LC}$  in most cases. The largest solute transport depths were predicted when the increases in precipitation was higher than the increase in potential evapotranspiration.

One way of assessing the likelihood for changes in the groundwater contamination risk is by summarizing the results for all future scenarios in all soils. Doing this for mid-century, we found that 33, 50 and 17% of the scenarios showed an increasing, unchanged and decreasing  $z_{COM}$ , respectively. For the end of the century, the equivalent numbers were 53, 39 and 8%. If the same data were analysed separately for each soil type, we see that clay and loam behave the same, but the sand soil is slightly more prone to increasing  $z_{COM}$  for both mid and end-century. If we instead summarize the data for each location, we see a clear difference. In Malmö, 50, 0 and 50% of the scenarios showed an increasing, unchanged and decreasing  $z_{COM}$ ,

respectively, for mid-century. By the end of the century the corresponding values were 50, 25 and 25%. Thus, the changes were small and the number of scenarios giving an increased risk were not increasing. In Petisträsk, 0, 75 and 25% of the scenarios showed an increasing, unchanged and decreasing  $z_{\text{COM}}$  for mid-century, for the end-century these values changed to 75, 25 and 0%. Norrköping showed an intermediate pattern. In other words, the groundwater contamination risk seems to increase more for higher latitudes in Sweden.

In order to investigate the effects of changes in precipitation and potential evapotranspiration and its effects on solute transport we calculated the absolute change in the difference between seasonal  $P$  and  $PET$ ,  $\Delta(P - PET)$  as:

$$\Delta(P - PET) = (P - PET) - (\overline{P}_h - \overline{PET}_h) \quad (2)$$

where  $\overline{P}_h$  and  $\overline{PET}_h$  are the average seasonal precipitation and potential evapotranspiration for the historical period, respectively. Using Equation (2), a yearly value of  $\Delta(P - PET)$  can be calculated, this was then compared to the absolute change in the difference between the yearly  $z_{\text{COM}}$  and  $z_{\text{LC}}$  calculated for the studied period and the average for the historical period;  $\Delta z_{\text{COM}} = z_{\text{COM}} - \overline{z_{\text{COM},h}}$  and  $\Delta z_{\text{LC}} = z_{\text{LC}} - \overline{z_{\text{LC},h}}$  respectively). In Fig. 5 we plot  $\Delta(P - PET)$  against  $\Delta z_{\text{COM}}$  for sand in Malmö as an example. This was the location exhibiting most scatter, but still there is a clear trend between  $\Delta(P - PET)$  and  $\Delta z_{\text{COM}}$ . In Fig. 5 a linear regression trend line ( $\Delta z_{\text{COM}} = 2.917\Delta(P - PET) + 111.35$ ,  $r^2 = 0.881$ ) is also plotted. Plots of  $\Delta z_{\text{LC}}$  were similar, as were those for other sites and soil types. In all cases, a linear trend fitted the data well for small changes in  $\Delta(P - PET)$ . However, at high  $\Delta(P - PET)$  ( $>250$  mm) or low  $\Delta(P - PET)$  ( $<-150$  mm) the linear relationship

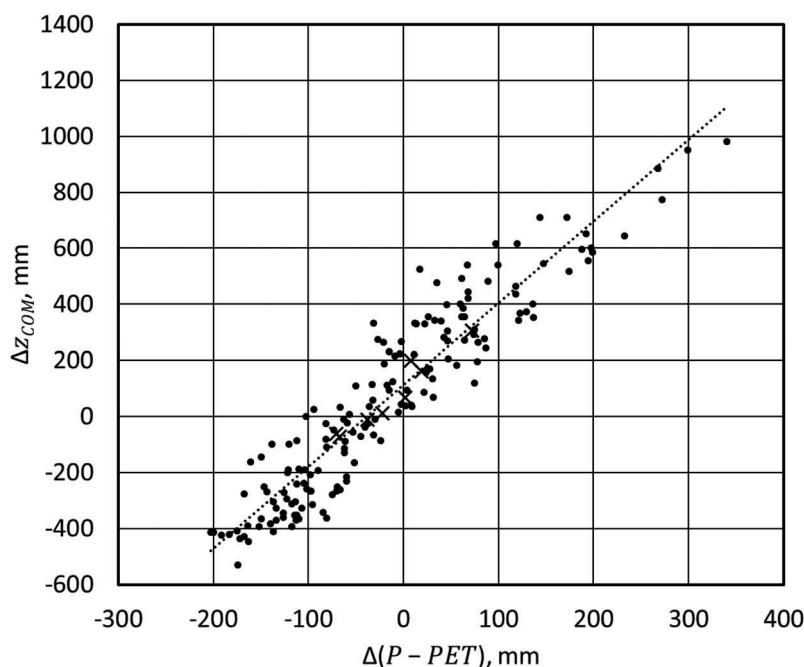
underestimated  $\Delta z_{\text{COM}}$  slightly, especially for clay. Thus, care should be taken when applying the linear trend for predicting  $\Delta z_{\text{COM}}$ .

Similar to (2), changes in average  $P - PET$  can also be defined as one value for each future scenario:

$$\Delta(\overline{P} - \overline{PET}) = (\overline{P} - \overline{PET}) - (\overline{P}_h - \overline{PET}_h) \quad (3)$$

where  $\overline{P}$  and  $\overline{PET}$  are the average precipitation and potential evapotranspiration for the future scenario, respectively. Using Equation (3),  $\Delta(\overline{P} - \overline{PET})$  can be calculated for each time period and can then be compared to the changes in the average  $z_{\text{COM}}$  and  $z_{\text{LC}}$  for each scenario and the average  $z_{\text{COM}}$  and  $z_{\text{LC}}$  for the historical period, e.g.  $\Delta \overline{z_{\text{COM}}} = \overline{z_{\text{COM}}} - \overline{z_{\text{COM},h}}$ . It is interesting to observe that only one (out of 24) studied future scenarios had a significantly positive  $\Delta(\overline{P} - \overline{PET})$  ( $p = 0.05$ ), while 10–11 future scenarios (out of 24) had a significantly positive  $\Delta \overline{z_{\text{COM}}}$  for each soil type. In other words, even in situations where the  $PET$  increase more than  $P$ , the groundwater contamination risk might increase. One explanation could be the increase in the high intensity precipitation events, a parameter that previously have been shown to be positively correlated to solute transport depths (Persson and Saifadeen 2016, Selim *et al.* 2017). This also means that the choice of DC method is a key factor. It is important that the DC method accurately mimics the relevant statistical characteristics for future scenarios, not only for mean precipitation over a given time period, but also the magnitude and frequency of extreme events. One such example, also mentioned above, is that the GCMs can predict lower summer totals but higher summer extremes. This must be accurately described by the DC method.

One should bear in mind that the number of future projections was limited in the present study. However, the linear



**Figure 5.** The absolute change in the difference between precipitation ( $P$ ) and potential evapotranspiration ( $PET$ ),  $\Delta(P - PET)$  plotted against  $\Delta z_{\text{COM}}$  for the sand in Malmö (circles), along with  $\Delta(\overline{P} - \overline{PET})$  plotted against  $\Delta \overline{z_{\text{COM}}}$  for the same dataset (crosses). The dotted line represents a linear regression for the  $\Delta(P - PET)$  to  $\Delta z_{\text{COM}}$  relationship.

relationship between  $\Delta(P - PET)$  and  $\Delta z_{COM}$ , could be used for calculating  $\Delta \bar{z}_{COM}$  for other scenarios with other values of  $\bar{P}$  and  $\overline{PET}$ . In Fig. 5 we show an example of this approach. In the figure the  $\Delta(\bar{P} - \overline{PET})$  and  $\Delta \bar{z}_{COM}$  for the eight scenarios for Malmö, sand is plotted. As can be seen, these data points follow closely the linear relationship. In other words, the linear relationship between  $\Delta(P - PET)$  and  $\Delta z_{COM}$  can be used to estimate  $\Delta \bar{z}_{COM}$  by calculating  $\Delta(\bar{P} - \overline{PET})$  for other scenarios, at least as long as the  $\bar{P}$  and  $\overline{PET}$  values are within the ranges found in the present study.

### Limitations and uncertainties

A study like the one presented here obviously has many uncertainties, in the emission scenarios, GCMs, RCM, DC method, solute transport model, etc. This needs to be taken into account when interpreting the results. The actual values of solute transport depths presented in the present study should not be overemphasized as no field validation of the model during a full season was conducted. Instead, the overall patterns of relative changes should be considered. As long as the uncertainties are kept in mind, we believe that our results can be used as a valuable guideline in assessing changes in the future groundwater contamination risk. Some specific limitations and their expected influence are discussed below.

Only non-adsorbing conservative solutes were considered in our study. A common example of such a pollutant is nitrate. Organic pollutants typically exhibits more or less strong sorption and will be transported slower. Our study can thus form a baseline for groundwater risk assessments. The modelling approach used in our study could also be extended to include both adsorption and degradation if the risks of a specific pollutant is to be assessed.

Our model only takes matrix flow into account. Especially in the clay soil macro pore flow is potentially of importance for a considerable amount of the solute transport. This means that the solute transport risk in clay soil might be underestimated in our study. Another limitation is that our model does not consider surface runoff and allowed for surface ponding. Surface runoff occurs when the rainfall intensity is larger than the infiltration capacity, which for saturated soils is equal to  $K_s$ . This do happen for a few 30-min time steps, but with only one exception, this never happens during two consecutive time steps. The exception was during one of the years during end-century in Malmö for CNRM8.5 in the clay soil, where the rainfall intensity was higher than  $K_s$  for two consecutive time steps. Since the agricultural land in Sweden is situated in plains with mild slopes, even if surface runoff is generated, most of it will be retained within the agricultural field to infiltrate as soon as the rainfall intensity decreases below  $K_s$ . Thus, surface ponding is expected to accurately model the actual real-world processes.

Due to the method chosen to handle evapotranspiration for the future scenarios, we were only able to produce one time series for each future period and RCP. This time series represents the average output of nine different climate models. In our study, the CNRM model consistently predicted higher temperatures compared to the EC model for the same

RCP. This means that evapotranspiration probably was underestimated for the scenarios using rainfall input from the CNRM model and overestimated for the scenarios forced by the EC model. In turn, this would mean that solute transport depth is overestimated in the CNRM scenarios and underestimated in the EC scenarios.

### Summary and conclusion

The groundwater contamination risk was assessed by simulating the transport depth at the end of the growing season for a conservative tracer added at the soil surface at the beginning of the growing season using HYDRUS-1D. The deeper (or equivalently, faster) the solutes are transported, the higher the risk for ground water contamination. Three different soil types at three different locations in Sweden were investigated. For each location and soil type, simulations were made for nine 20-year periods, one historical (1996–2015) and eight future projections. For the future projections, we used precipitation data from two GCMs using two RCPs each and two time periods representing mid- and late-century, respectively. Potential evapotranspiration used was calculated from an ensemble of nine GCMs for three emission scenarios.

Results showed that most future scenarios was predicted to have a significantly higher precipitation, up to 35% higher compared to the historical period. The potential evapotranspiration was predicted to increase with up to 25%. The net change in the difference between precipitation and potential evapotranspiration, however, decreased in 75% of the future projections.

Simulated solute transport depths varied substantially between different future projections, from – 10% to +45% for  $z_{COM}$  and – 8% to +23% for  $z_{LC}$ . Both the largest increases and decreases were found in southern Sweden. For mid-century, 33, 50 and 16% of the scenarios showed an increasing, unchanged and decreasing groundwater contamination risk, respectively. For the end of the century, the values were 53, 39 and 8%, respectively. In Malmö, the groundwater contamination risk will increase to the mid-century and the only increase slightly further for end-century. In Petisträsk, the groundwater contamination risk remains more or less unchanged until mid-century and then increase until end-century. There were only small differences between the soil types, however, sand showed a slightly higher likelihood of increased groundwater contamination risk in the future.

A high correlation between  $\Delta(P - PET)$  (absolute change in the difference between precipitation ( $P$ ) and potential evapotranspiration ( $PET$ )) and changes in  $z_{COM}$  and  $z_{LC}$  were found for each soil type and location.

One should note that the output of different GCMs, emission scenario and downscaling method result in very different values of  $z_{COM}$  and  $z_{LC}$ . The values presented here should be viewed as possible changes in  $z_{COM}$  and  $z_{LC}$  and results should not be considered to represent actual future changes. The derived relationships between  $\Delta(P - PET)$  and changes in  $z_{COM}$  and  $z_{LC}$  could be used for estimation of solute transport depth changes for other future scenarios with other values of precipitation and potential evapotranspiration.

It should be noted that the results applies to conservative point source pollutions spread at the soil surface at the beginning of the growing season. A complete analysis of groundwater contamination risks would have to also involve the winter season with frozen soils and snow and snowmelt processes. This was, however, beyond the scope of the present study, but will be further investigated in the future.

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